

# Heat load for a beam loss on the superconducting magnet

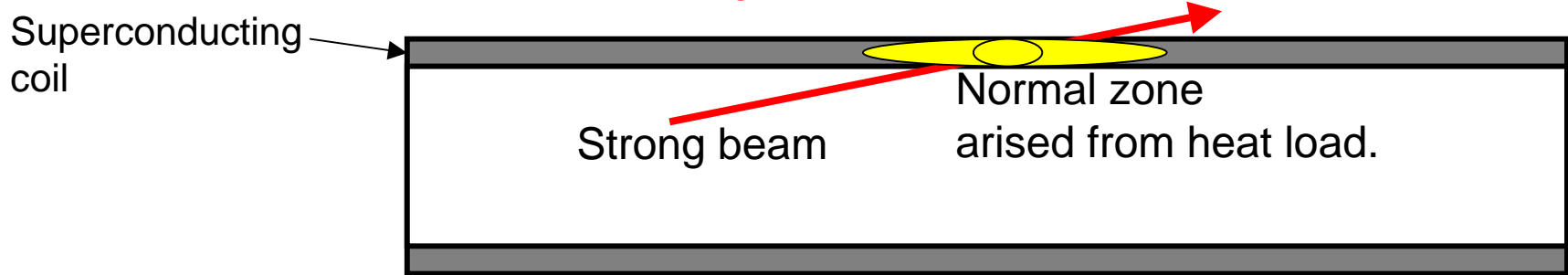
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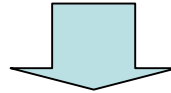
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# Introduction

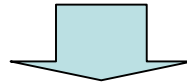
“**Quenching**” occurs when any part of a magnet goes from the **superconducting** to the **normal resistive state**.



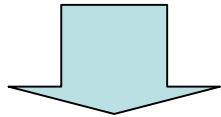
Investigate the quench stability of the superconducting cables



In case of **50GeV-10W/point beam loss**  
(in view of radiation shielding and maintenance)

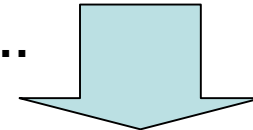


**Heat load** on the cable was calculated using **MARS** code.



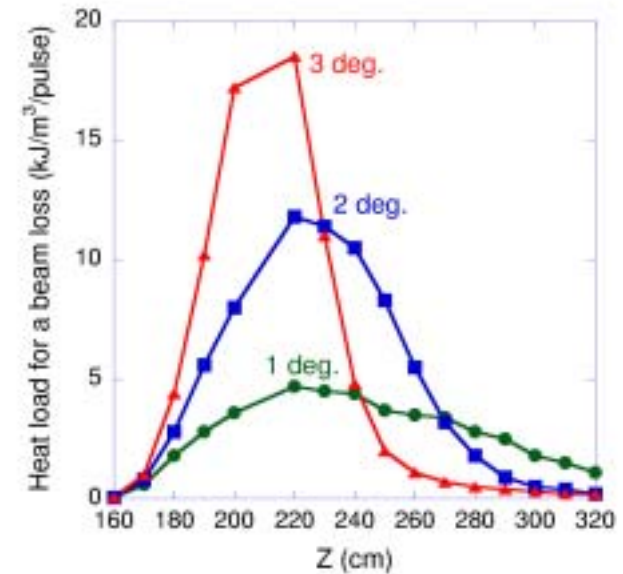
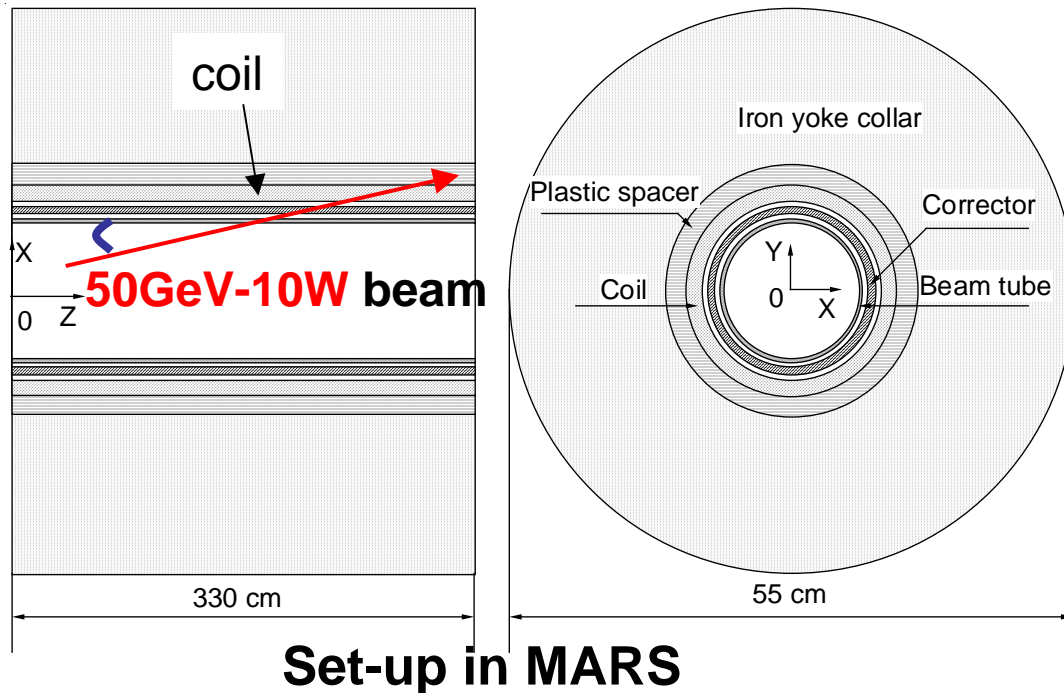
**Measurements**  
of temperature rise of the cable

Using calculated heat load.....



**Quench stability simulation**<sub>2</sub>

# Calculation of heat load on the coil– for a 10 W/point loss by using MARS code.



**Heat load on the coil**

Heat load will be up to **20 kJ/m<sup>3</sup>/pulse**.

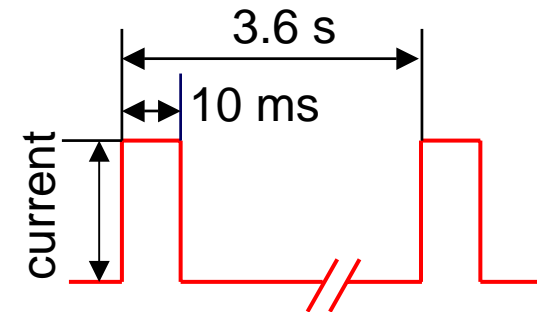
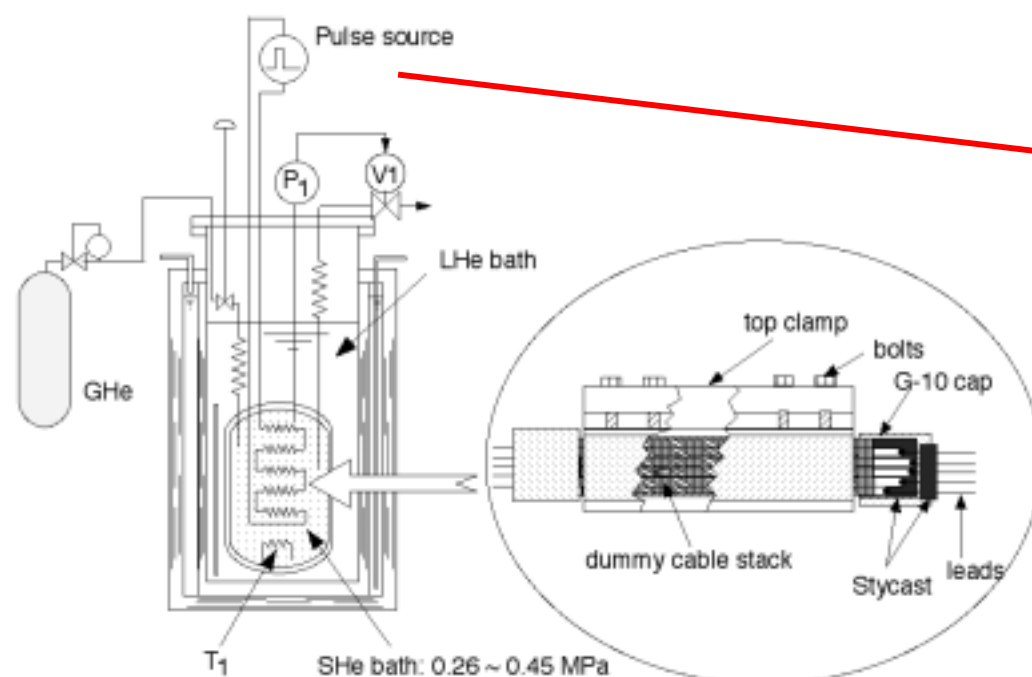
Heating of **0-40 kJ/m<sup>3</sup>/pulse** was used in measurement and the quench simulation.

# Measurement of temperature rise of the cable

It is **difficult** to make an experiment **using actual beam**.

The **cable** was heated with a **pulse generator**.

The **cable** was used **the same structure** of **LHC** superconducting magnet.



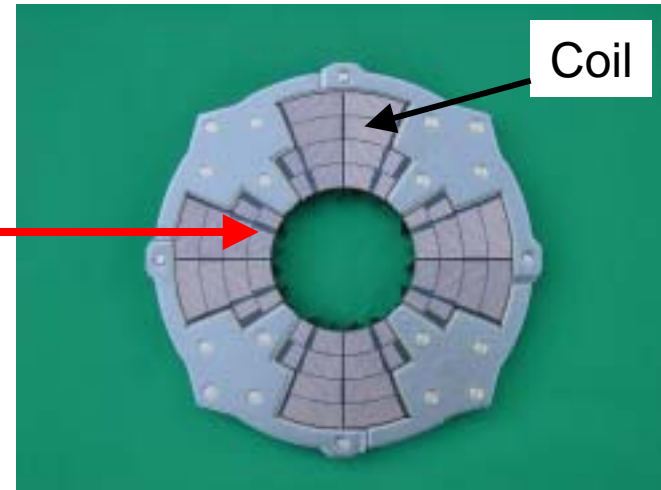
Heat load (kJ/m<sup>3</sup>/pulse) **8, 14, 20, 28, 37**  
Current (A) 30, 40, 50, 60, 70

P<sub>1</sub>: Absolute pressure transducer

T<sub>1</sub>: Silicon diode thermometer

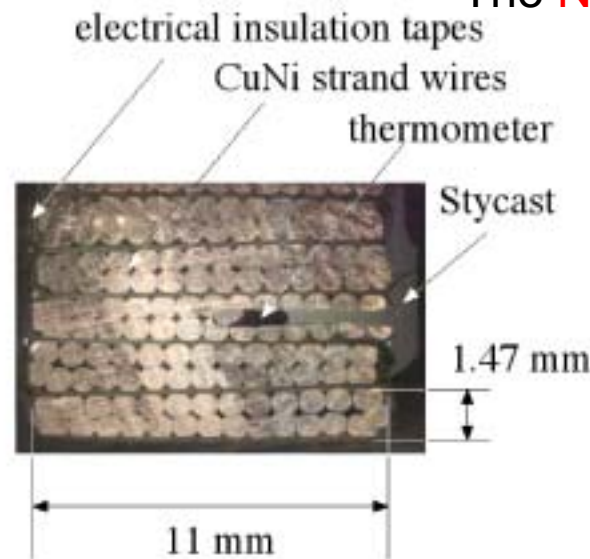
V<sub>1</sub>: Pressure control valve

The **cable** that is used for the coil of the **LHC** magnets will be used for the **J-PARC** coil.



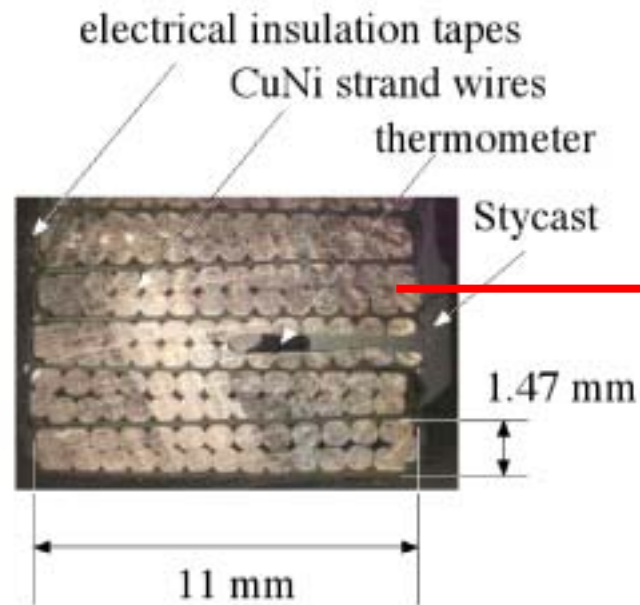
The LHC insertion region quadrupole, MQXA magnet

Cross section of the MQXA magnet.  
The **NbTi/Cu** strand wires are used.



Cross section of the cable using this work .

The **CuNi** strand wires were used in order to generate **Joule heating**.  
However, This cable is **same structure** of the coil stack for the **MQXA magnet**.



**Cross section of the cable**

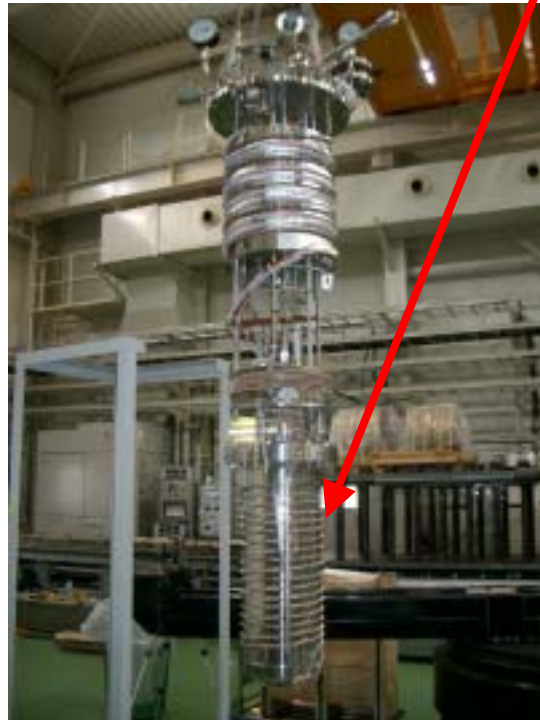


**Specimen**

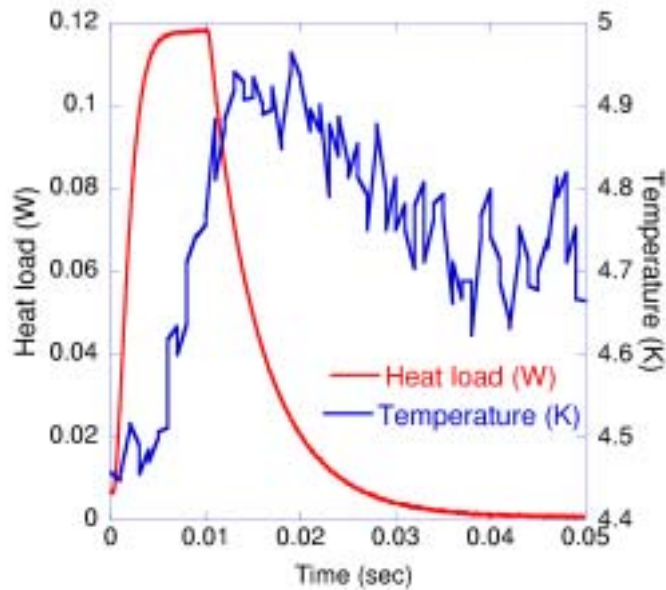
It was installed in supercritical helium bath.  
(4.4 K, 0.3 MPa)

## Overview

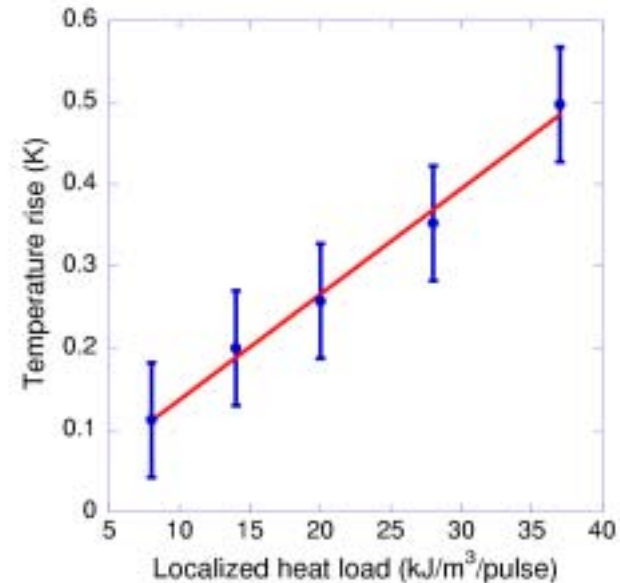
It was installed in cryostat.



# Experimental result



**28 kJ/m<sup>3</sup>/pulse** heat load.  
**0.46 K** temperature rise.



Temp. rise is proportional to heat load.

**20 kJ/m<sup>3</sup>/pulse** (for a **50GeV-10W** beam loss)



Instantaneous temp. rise = **0.25 K**



# Quench Stability Simulation

Heat balance equation

$$A \frac{d}{dx} \left( k(T) \frac{dT}{dx} \right) - P q_s + gA = AC_p(T) \frac{dT}{dt}$$

$A$ : the overall cross section

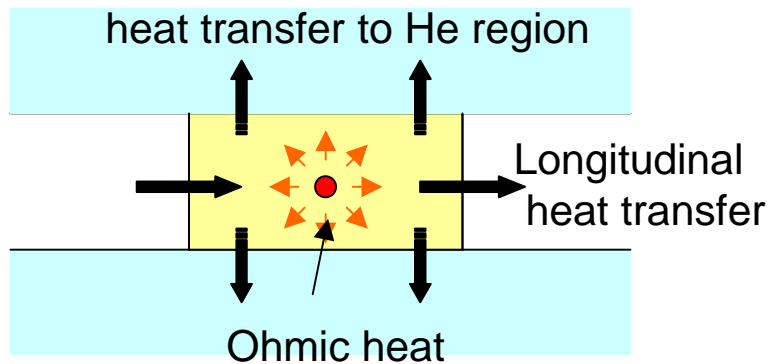
$K(T)$ : thermal conductivity of conductor

$P$ : strand's wetted perimeter

$q_s$ : heat transfer to SHe

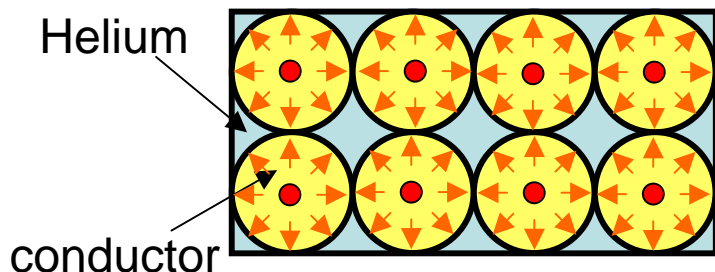
$g$ : Joule heating in conductor

$C_p(T)$ : volumetric specific heat of conductor

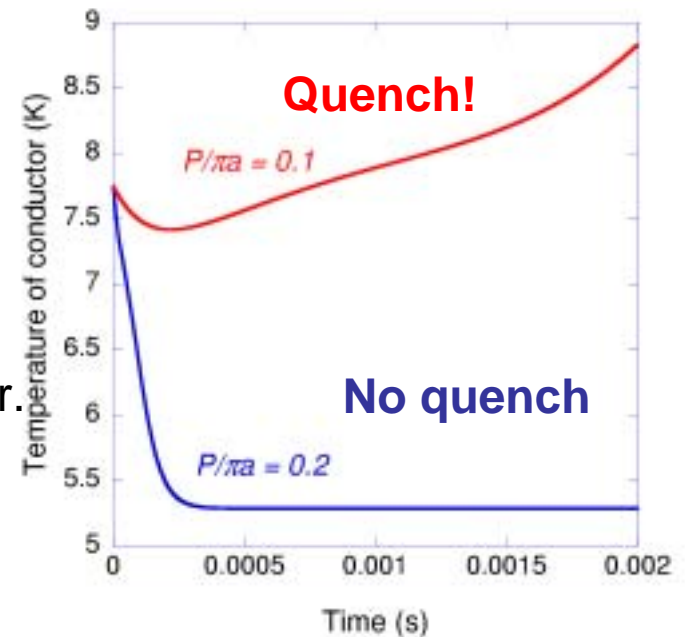


Quench tends to be influenced on parameter,  $p/\pi a$ .

$p/\pi a$  indicates the contact ratio with He and conductor.

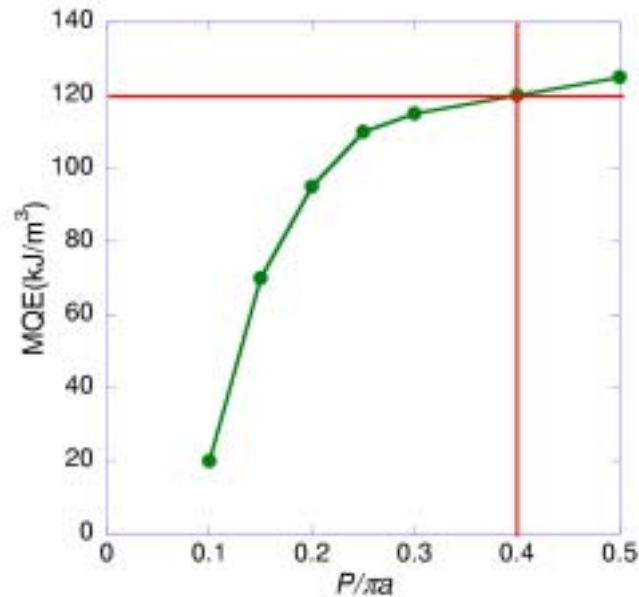


Cross section of the cable.



Simulation result of temp. versus time.  
20kJ/m<sup>3</sup> heat load into conductor

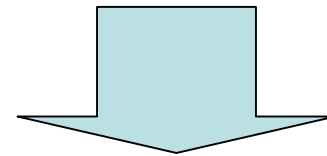




**Stability margin.**

**$P/\pi a \sim 0.4$  (the actual cable)**

**20 kJ/m³/pulse** heat load is **OK**  
(for a **50GeV-10W** beam loss)



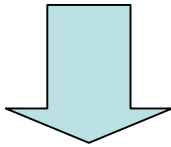
**120 kJ/m³/pulse** heat load  
(for a **50GeV-60W** beam loss)  
may be **acceptable.**

MQE is minimum quench energy.

**$p/\pi a$**  is the contact ratio with He and conductor.

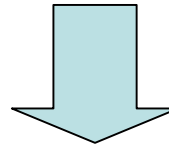
# Summary

Heat load on the coil will be up to **20 kJ/m<sup>3</sup>/pulse** for a **10W/point beam loss** by **MARS** code.



## Experimental result

Instantaneous temp. rise  
in the cable = **0.25 K**



## Quench simulation result

**Not** induce a **quench**.  
At least,  
**120 kJ/m<sup>3</sup>/pulse** heat load  
for a **50GeV-60W** beam loss  
may be **acceptable**.